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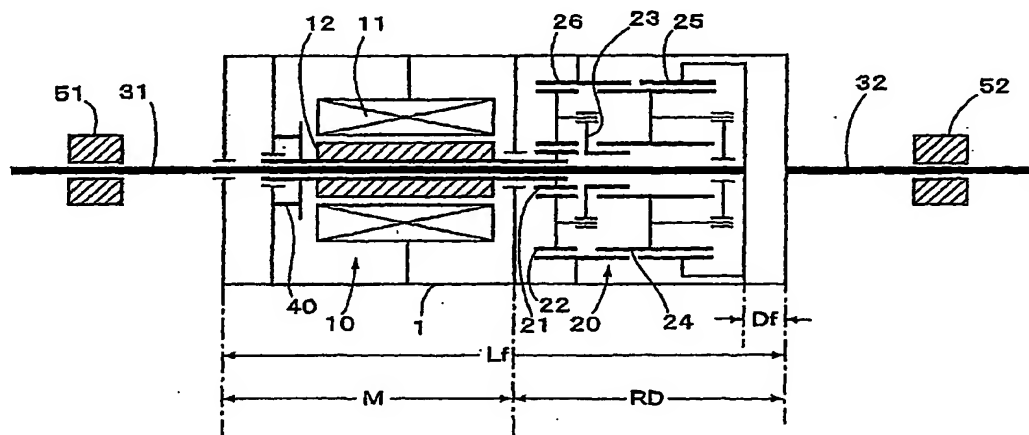
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(54) Title: STABILIZER CONTROL DEVICE FOR VEHICLE



(57) Abstract: A stabilizer control device for vehicle includes a pair of stabilizer bars (31, 32) provided between a left wheel and a right wheel of a vehicle, and an actuator including a reduction mechanism (RD) connecting between said pair of stabilizer bars (31, 32) and a motor (M) connected to the reduction mechanism (RD) for providing torsion force to said pair of stabilizer bars (31, 32) through the reduction mechanism (RD) wherein the reduction mechanism (RD) comprises a first gear (25) and a second gear (26) for generating relative rotational speeds differential therebetween, the first gear (25) and the second gear (26) are coaxially placed adjacent to each other, and opposed side faces of stabilizer bars (31, 32) are adjacently connected with the first gear (25) and the second gear (26) respectively and disposed in the reduction mechanism (RD).

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For two-letter codes and other abbreviations, refer to the "Guidance Notes on Codes and Abbreviations" appearing at the beginning of each regular issue of the PCT Gazette.

Stabilizer control device for vehicle

FIELD OF THE INVENTION

5 The present invention generally relates to a stabilizer control device for vehicle. More particularly, the present invention pertains to a stabilizer control device for vehicle which controls torsion force of a stabilizer device disposed between left and right wheels of a vehicle.

BACKGROUND OF THE INVENTION

10

A stabilizer control device for a vehicle commonly gives appropriate roll moment to a stabilizer bar provided between left and right wheel of the vehicle while turning travel. As an example to realize this function, a disclosed Japanese
15 Patent Laid-open Publication No.2002-518245 has been proposed. In this disclosed document, a roll stabilizer device for a vehicle has been constructed wherein an electromechanical rotating actuator is disposed between a pair of stabilizer bars. Additionally, a motor and a reduction gear device are interposed between said pair of stabilizer bars. The reduction gear device is made of a
20 common multistage planetary gear mechanism.

In above mentioned roll stabilizer device of a vehicle, the motor and the reduction gear device are provided as a unit which is referred to as an actuator. The length of each divided stabilizer bar with the actuator system is shorter than
25 that of previous type (i.e. non divided, a single stabilizer bar) without actuator system as much as width direction length of the actuator. Accordingly, compared with the single stabilizer bar, the thickness of the divided stabilizer bar turns into thick to ensure the torsion force necessary only by the stabilizer bar while the actuator does not work.

30

Thus, whole the stabilizer system becomes larger and heavier. This causes restriction for mounting to vehicle since one side of stabilizer bar will be attached

to a suspension member.

As an example of a reduction mechanism for providing large reduction ratio, a Ferguson Mechanical Paradox has been published on "Kikougaku" by K. Ogawa and I. Katoh, 1st. edition, 7th print, Morikita Shuppan Co. Ltd. pages.164-165 (March 1, 1976). As another example of a reduction mechanism, a harmonic drive mechanism (which is the trademark of Harmonic Drive Systems, Inc.) has been opened on the web site http://www.hds.co.jp/HDS_hp_english/english/hd/index.html (retrieved on February 13, 2004).

DISCLOSURE OF THE INVENTION

In light of foregoing, according to an aspect of the present invention, a stabilizer control device for vehicle includes a pair of stabilizer bars disposed between a left wheel and a right wheel of a vehicle, and an actuator including a reduction mechanism connecting said pair of stabilizer bars and a motor connected to the reduction mechanism for providing torsion force to said pair of stabilizer bars through the reduction mechanism wherein the reduction mechanism comprises a first gear and a second gear for generating relative rotational speeds differential therebetween, the first gear and the second gear are coaxially placed adjacent to each other, and opposed side faces of stabilizer bars are adjacently connected with the first gear and the second gear respectively and disposed in the reduction mechanism.

It is preferable that the first gear and the second gear include a pair of internal tooth gears with different number of teeth, and a common planetary gear train is engaged with both internal tooth gears.

It is preferable that the first gear and the second gear are cooperatively associated with each other.

It is preferable that the motor is a brush-less motor with a rotor and a stator, and one of the pair of stabilizer bar is integrally attached to the first gear through the rotor.

- 5 It is preferable that the motor and the reduction mechanism are disposed in a housing, and the other of the pair of stabilizer bar is integrally attached to the housing.

- 10 It is preferable that the motor and the reduction mechanism are disposed in a housing, and the one of the pair of stabilizer bars connected to the first gear passing through the rotor is supported at both sides of the motor and the first gear.

- 15 It is preferable that the one of the stabilizer bar is attached to the housing by spline connection.

It is preferable that the planetary gear train includes plural planetary gear sets.

- 20 It is preferable that the planetary gear train is a multistage planetary gear.

It is preferable that a rotation detection means is disposed in the housing for detecting rotation of at least one of the stabilizer bars.

BRIEF DESCRIPTION OF THE DRAWINGS

25

The foregoing and additional features and property of the present invention will become more apparent from the following detailed description considered with reference to the accompanying drawing figures wherein:

- 30 FIG. 1 is a plane view schematically illustrating a vehicle comprising a stabilizer control device according to the first embodiment of the present invention;

FIG. 2 is a perspective view schematically illustrating a conformation example of an actuator according to the first embodiment of the present invention;

FIG. 3 is a cross sectional skeleton figure of an actuator according to the first
5 embodiment of the present invention;

FIG. 4 is a cross sectional view of an actuator according to the first embodiment of the present invention;

10 FIG. 5 is a cross sectional view taken along line A-A in FIG.4;

FIG. 6 is a cross sectional skeleton figure of an actuator according to the second embodiment of the present invention;

15 FIG. 7 is a partial cross sectional view of an actuator according to the second embodiment of the present invention; and

FIG. 8 is a cross sectional skeleton figure of an actuator wherein the actuator construction explained in the background of the invention is alternated to
20 construction of the first embodiment of the present invention.

DETAILED DESCRIPTION OF PREFERRED EMBODIMENTS

A preferred embodiment of the present invention will be described hereinbelow
25 in detail with reference to the accompanying drawings.

A first embodiment of the present invention is explained referring to FIGs. 1 to 5. As shown in FIG. 1, a front stabilizer SB_f and a rear stabilizer SB_r are disposed at front wheel side and rear wheel side of a vehicle body (not shown),
30 respectively. Each stabilizer SB_f, SB_r works as a torsion spring when a roll directional motion is supplied to the vehicle. Also, each stabilizer is constructed to control variable torsion force using a stabilizer actuator (hereinafter referred to

as an actuator) FT, RT. In addition, actuators FT, RT are controlled by a stabilizer control unit ECU1 provided in a electronic control unit ECU.

As shown in FIG. 1, wheel speed sensors WSfr, WSfl, WSrr, and WSrl are disposed at front right wheel, front left wheel, rear right wheel, and rear left wheel. Each wheel speed sensors are connected to the electronic control unit ECU to input a signal with respect to a wheel rotation speed, respectively. A steering sensor SA for detecting steering angle of a steering wheel SW, a X acceleration sensor XG for detecting an acceleration with forward and backward movement, a Y acceleration sensor YG for detecting an acceleration in a vehicle width direction, and a yaw rate sensor YR for detecting yaw rate of the vehicle are connected to the electronic control unit ECU.

The electronic control unit ECU includes a brake control unit ECU2, a steering control unit ECU3 in addition to the stabilizer control unit ECU1. These control units ECU1, ECU2 and ECU3 are connected to a communication bus through a communication unit (not shown) including a CPU, ROM, and RAM.

FIG. 2 shows composition of the front stabilizer SBf. The rear stabilizer SBr has similar configuration to the front stabilizer SBf. One end of each stabilizer bar 31, 32 is connected to the right and left wheels in the vehicle, respectively. The other end of each stabilizer bar 31, 32 is connected to an actuator FT which will be explained in detail later. The stabilizer bars 31, 32 are held on vehicle body by using holding means 51, 52.

Each actuator FT, RT (hereinafter represented as FT) includes a motor M and a reduction mechanism RD, respectively. FIG. 3 is an example of the actuator FT. In the first embodiment, a three-phase brushless motor is used as the motor M. Although configuration of the motor M is not only limited to the three-phase brushless motor, but also another type of motor (for example, common motor including brush, and another phase number) may be used.

Accordingly, in the stabilizer ECU1, target value of active roll moment is set for each front and rear wheel based on vehicle active roll moment set value and front/rear wheel roll torsion modulus set value for active control of vehicle roll moment. According to this target value of active roll moment, torsion stress for generating at front (and/or rear) actuator FT (and/or RT) is determined. Then, the motor is activated in controlled to reach the determined torsion stress. By making active work to control the torsion force to each stabilizer bar 31, 32 with the actuator FT, vehicle roll can be reduced or inhibited when the vehicle is driven. Although control method of the stabilizer is not only limited to the embodiment described, but also another method (for example the method described in the disclosed Japanese Patent Laid-open Publication No. 2002-518245, cited above) may be used.

Next, configuration of the actuator is explained in detail. An embodiment applicable to an actuator, which gives torsion force to each actuator FT and RT, is explained since actuators FT and RT are substantially same composition as shown in FIG. 1. FIG.3 and FIG. 4 are a skeleton figure and a concrete cross sectional figure, respectively. In these figures, a brushless type DC motor 10 is used as the motor M, and a Furguson Mechanical Paradox 20 is used as a reduction mechanism, and corresponding elements are expressed as same number. The motor 10 and the Furguson Mechanical Paradox 20 are integrally composed, and accommodated in a housing 1.

For the Furguson Mechanical Paradox 20, the stabilizer bar 31 is rigidly connected to a ring gear 25 (first gear). Also, the stabilizer bar 32 is rigidly connected to a ring gear 26 (second gear). The actuator side of each stabilizer 31, 32 is placed adjacent to each other in the reduction mechanism RD in the housing 1. Namely, opposed side faces of stabilizer bars 31, 32 are placed with distance Df therebetween as shown in FIG. 3 and FIG. 4. To be more precise, as shown in FIG. 4, the stabilizer bar 31 is fixed to an endplate 25e integrally formed with the ring gear 25. On the other hand, an endplate 32e integrally formed with the stabilizer bar 32 are fixed to the housing 1 (for example, spline

connection may be applied to fix). Accordingly, the stabilizer bar 32 is integrally jointed to the ring gear 26 since the ring gear 26 is integrally formed with the housing 1 interior side.

5 Two ring gears 25, 26 are internal tooth gears with different number of teeth thereof (for example, number of teeth; 60 and 62). As a common planetary gear engaging with each ring gear 25, 26, three planetary gears 24 are movably supported around an axis of the stabilizer bar 31. In consideration of specification of the motor 10 and reduction ratio of the reduction mechanism RD,
10 two-stage planetary gear is used in the present embodiment. As shown in FIG. 5 which is cross sectional view taken along A-A of FIG. 4, a sun gear 21 fixed to a rotor 12 of the motor 10 is provided to engage with three first-stage planetary gears (represented as 22).

15 The first-stage planetary gears 22 are rotatably supported by a sun gear 23 and rotatably supported around an axis of the stabilizer bar 31 (namely, rotational axis of the sun gears 21 and 23). These first-stage planetary gears 22 are engaged with the sun gear 21, and also the ring gear 26. Accordingly, the first-stage planetary gears 22 are rotatably supported between the sun gear 21 and
20 the ring gear 26 as if they play sun-and-planet motion with an axis of the stabilizer bar. Second-stage planetary gears 24 are engaged with the sun gear 23 and the ring gear 25, 26. Accordingly, the second-stage planetary gears 24 rotate between the sun gear 23 and each ring gear 25, 26 as if they also play sun-and-planet motion with an axis of the stabilizer bar.

25

On the other hand, the motor 10 includes a stator 11 and a hollow rotor 12, as shown in FIG. 3. As shown in FIG. 4, the rotor 12 is a hollow cylindrical shape so as to surround corresponding part of the stabilizer bar 31 and rotatably supported by interior of the housing 1 and a cap member 2 of the housing 1 at
30 bearing 12b disposed at each sides of the rotor 12. The rotor 12 includes multipolar magnets (not shown). The stator 11 is fixed to interior of the housing 1 so as to surround the rotor 12.

The stabilizer bar 31, which is fixed to the ring gear 25 as one side thereof, is rotatably supported at interior of the housing 1 through a bearing 31a. The stabilizer bar 31 is rotatably supported at inferior of the cap member 2 on contact with the bearing 31b at outside of the motor 10. Although the cap member 2 is formed as a different member to the housing 1, the cap member 2 may be integrally formed with the housing 1. The housing 1 expressed in the first embodiment is composed herewith. Namely, in the first embodiment, the one of the pair of stabilizer bars (stabilizer bar 31) connected to the first gear (ring gear 25) passing through the rotor 12 is supported at both the motor 10 side and the first gear (ring gear 25) side in the housing (the housing 1 and the cap member 2). Then, a bending moment to become load can be adequately shared by the stabilizer bar 31, the housing 1 and the cap member 2, and ring gears 25, 26.

In addition, a rotation detection mean 40 for detecting rotation of the stabilizer bar 31 is disposed in the housing 1. Although the rotation detection mean 40 comprises at least one magnet 41 provided along outer circumferential of the rotor 12 and at least one hall IC 42 disposed at interior of the housing 1 in the present embodiment, another type of the rotation detection mean (for example, optical rotary encoder) may be used.

As shown in FIG.3, according to the first embodiment, the housing side of each end of stabilizer bar 31, 32 is placed in the vicinity of each other, and the distance D_f therebetween is shorter than overall length L_f of the housing 1. Accordingly, the stabilizer 31, 32 can have almost the same overall length compared with a non-divided stabilizer (without actuator). The stabilizer bar can be formed same material with same diameter and weight compared with common stabilizer (without actuator). Then, design flexibility can be extended in vehicle width direction.

On the other hand, the composition of the motor M and reduction mechanism RD of the first embodiment may be applied to an actuator described in the

background of the present invention. Namely, one end of each stabilizer bar 31, 32 is connected to the housing 1x (for the stabilizer bar 31) and the reduction mechanism RD (for the stabilizer bar 32), respectively. In this configuration, the stabilizer bar 31, 32 can be made to be longer than the configuration using multistage planetary gear mechanism explained in the background of the invention. Although, the length of each stabilizer bar 31, 32 is shorter than the stabilizer bar of the first embodiment since the distance between both connection points (one end) of the stabilizer bars 31, 32 ($L_m + L_r$) is longer than that of the first embodiment (D_f).

Next, a second embodiment of the present invention is explained referring to FIG. 6 and FIG. 7. In the second embodiment, a harmonic drive type gear mechanism (hereinafter referred to as gear mechanism) 60 is applied as a reduction mechanism RD. FIG. 6 is a skeleton figure, and FIG. 7 is a concrete cross sectional figure. Corresponding elements are expressed as same number.

For the gear mechanism 60, the stabilizer bar 31, 32 are integrally connected to a flexible gear 62 and a ring gear (second gear) 63, respectively. The flexible gear 62 is expressed as "flexpline" in the opened website described in the background of the invention. Also, the ring gear 63 is expressed as "circular spline". In the second embodiment, stabilizer bar 31, 32 end faces are placed with distance D_h therebetween as shown in FIG. 6 and FIG. 7.

To be more precise, as shown in FIG. 7, the stabilizer bar 31 is supported by an end portion 62c of the flexible gear 62 via a bearing 31c with rotatable condition. Additionally, an end portion 32c integrally formed with the stabilizer bar 32 are fixed to the housing 1h (for example, spline connection is applied to fix). Then, the stabilizer bar 31 is inserted passing through the rotor 12 (abbreviated in FIG. 7), and supported at the end portion 62c of the flexible gear 62 so as to rotate to the housing 1h. On the other hand, the stabilizer bar 32 is integrally jointed to the ring gear 63 since the ring gear 63 is integrally formed with the housing 1h interior side (see FIG. 6). The rotor 12 of the motor 10 is fixed to an elliptic gear

61 and cooperated with the flexible gear 62. The elliptic gear 61 is expressed as "wave generator" in the opened website described in the background of the invention. Then, in the second embodiment, one of the pair of stabilizer bar (stabilizer bar 31) connected to the first gear 62 (end portion 62c) through the rotor 12 (abbreviated in FIG. 7) is supported at both the motor 10 side (abbreviated in FIG. 7) and the first gear 62 (end portion 62c) side in the housing 1h. Then, a bending moment to become load can be adequately shared as well as the first embodiment thereof.

In above mentioned website, function of the elliptic gear 61, the flexible gear 62 and the ring gear 63 is explained below. The elliptic gear 61 corresponding to the "wave generator" is a component having small ball bearings built into the outer circumference of the elliptical cam. The outer raceway is subjected to elastic deformation via the ball bearings. The flexible gear 62 corresponding to the "flexspline" is a thin cup-shaped metal rim component with external teeth. The ring gear 63 corresponding to the "circular spline" is a rigid body ring with internal teeth. The ring gear 63 has two teeth more than the flexible gear 62. For example, when the elliptic gear 61 is rotationally activated with attaching the elliptic gear 61 to the rotor 12 of the motor 10, and attaching the flexible gear 62 to the stabilizer bar 31, rotation of the flexible gear 62 is transmitted to the ring gear 63 engaged with the flexible gear 62. The ring gear 63 rotates opposite rotation direction relative to the rotation of the flexible gear 62, and rotation of the ring gear 63 is reduced since it has two teeth more than the flexible gear 62.

As shown in FIG.6 and FIG. 7, according to the second embodiment, actuator side of each stabilizer bar 31, 32 is placed close to each other, and the distance D_h therebetween is shorter than overall length L_h of the housing 1h. Accordingly, the stabilizer bars 31, 32 can have almost the same overall length compared with a non-divided stabilizer (without actuator). The stabilizer bars 31, 32 can be formed same material with same diameter and weight compared with common stabilizer (without actuator). In particular, overall length L_h of the housing 1h for the second embodiment can be formed shorter than that (L_f) of the first

embodiment. Then, further smaller sized actuator can be made.

The principles, a preferred embodiment and mode of operation of the present invention have been described in the foregoing specification. However, the
5 invention which is intended to be protected is not to be construed as limited to the particular embodiment disclosed. Further, the embodiment described herein is to be regarded as illustrative rather than restrictive. Variations and changes may be made by others, and equivalents employed, without departing from the spirit of the present invention. Accordingly, it is expressly intended
10 that all such variations, changes and equivalents which fall within the spirit and scope of the present invention as defined in the claims, be embraced thereby.

CLAIMS:

1 A stabilizer control device for vehicle, comprising:

a pair of stabilizer bars provided between a left wheel and a right wheel of a
5 vehicle; and

an actuator including a reduction mechanism connecting between said pair of
stabilizer bars and a motor connected to the reduction mechanism for providing
torsion force to said pair of stabilizer bars through the reduction mechanism;

wherein the reduction mechanism comprises a first gear and a second gear for
10 generating relative rotational speeds differential therebetween, the first gear and
the second gear are coaxially placed adjacent to each other, and opposed side
faces of stabilizer bars are adjacently connected with the first gear and the
second gear respectively and disposed in the reduction mechanism.

15 2 A stabilizer control device for vehicle according to claim 1, wherein the first
gear and the second gear include a pair of internal tooth gears with different
number of teeth, and a common planetary gear train is engaged with both
internal tooth gears.

20 3 A stabilizer control device for vehicle according to claim 1, wherein the first
gear and the second gear are cooperatively associated with each other.

4 A stabilizer control device for vehicle according to claim 1, wherein the
motor is a brush-less motor with a rotor and a stator, and one of the pair of
25 stabilizer bar is integrally attached to the first gear passing through the rotor.

5 A stabilizer control device for vehicle according to claim 4, wherein the
motor and the reduction mechanism are disposed in a housing, and the other of
the pair of stabilizer bar is integrally attached to the housing.

30 6 A stabilizer control device for vehicle according to claim 4, wherein the
motor and the reduction mechanism are disposed in a housing, and the one of

the pair of stabilizer bars connected to the first gear passing through the rotor is supported at both sides of the motor and the first gear.

7 A stabilizer control device for vehicle according to claim 6, wherein the other
5 of the pair of stabilizer bar is integrally attached to the housing.

8 A stabilizer control device for vehicle according to claim 6, wherein the one of the stabilizer bar is attached to the housing by spline connection.

10 9 A stabilizer control device for vehicle according to claim 2, wherein the planetary gear train includes plural planetary gear sets.

10 A stabilizer control device for vehicle according to claim 2, wherein the planetary gear train is a multistage planetary gear.

15

11 A stabilizer control device for vehicle according to claim 1, wherein a rotation detection means is provided in the housing for detecting rotation of at least one of the stabilizer bars.

FIG. 1

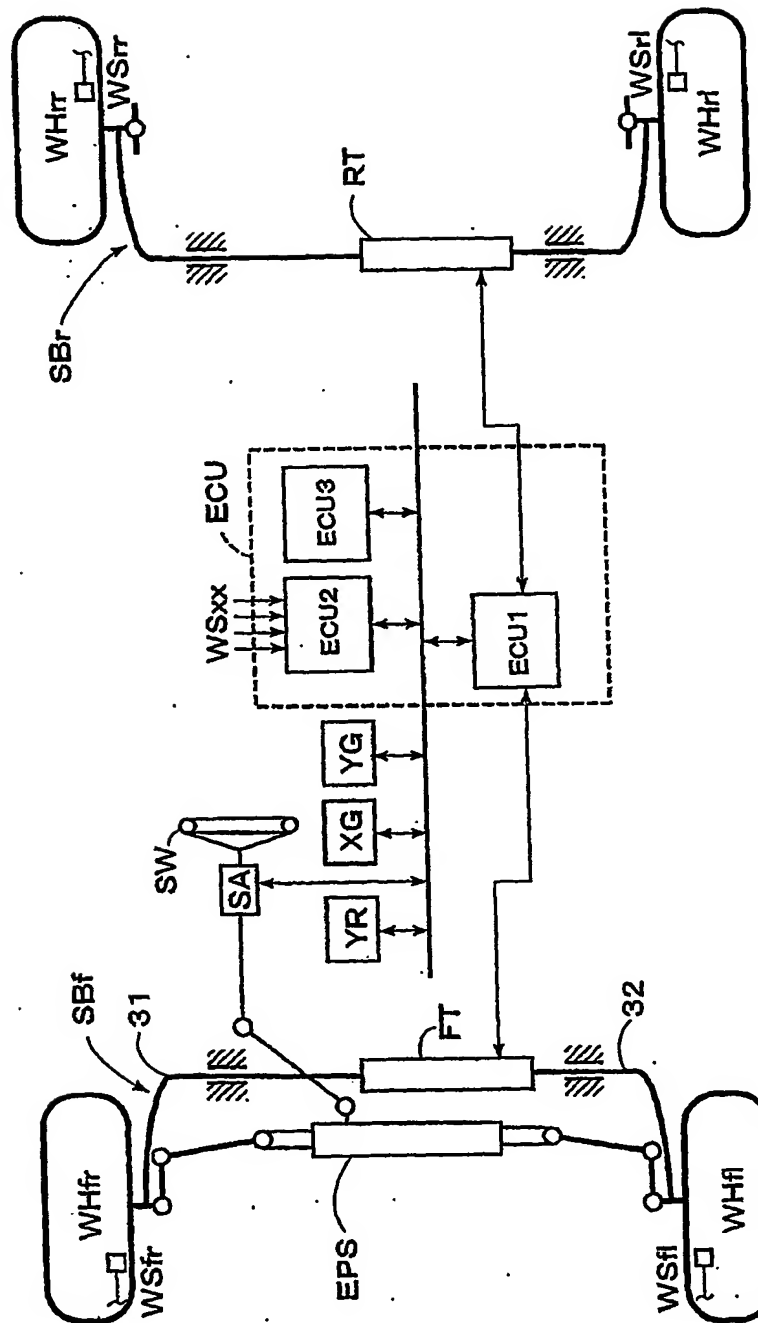


FIG. 2

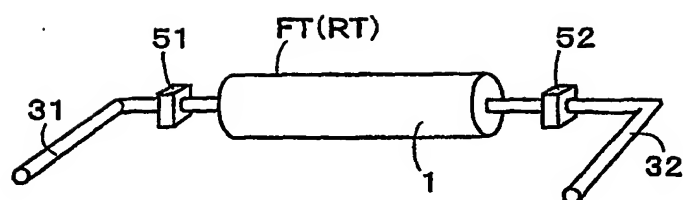


FIG. 3

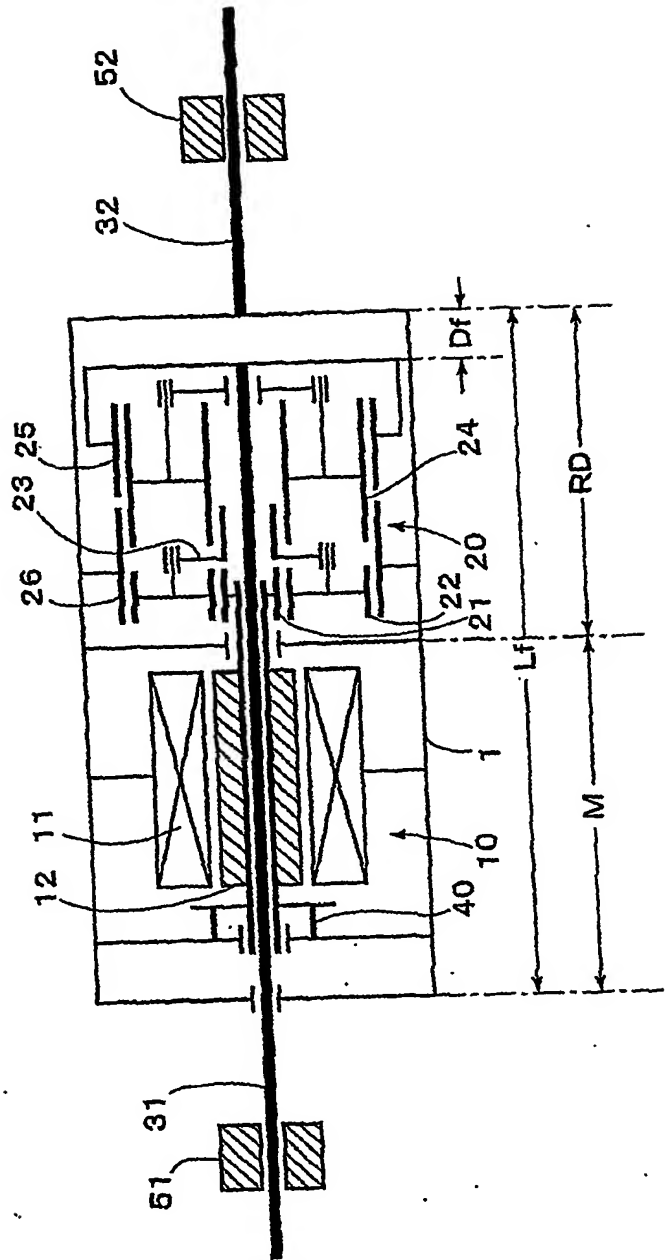


FIG. 4

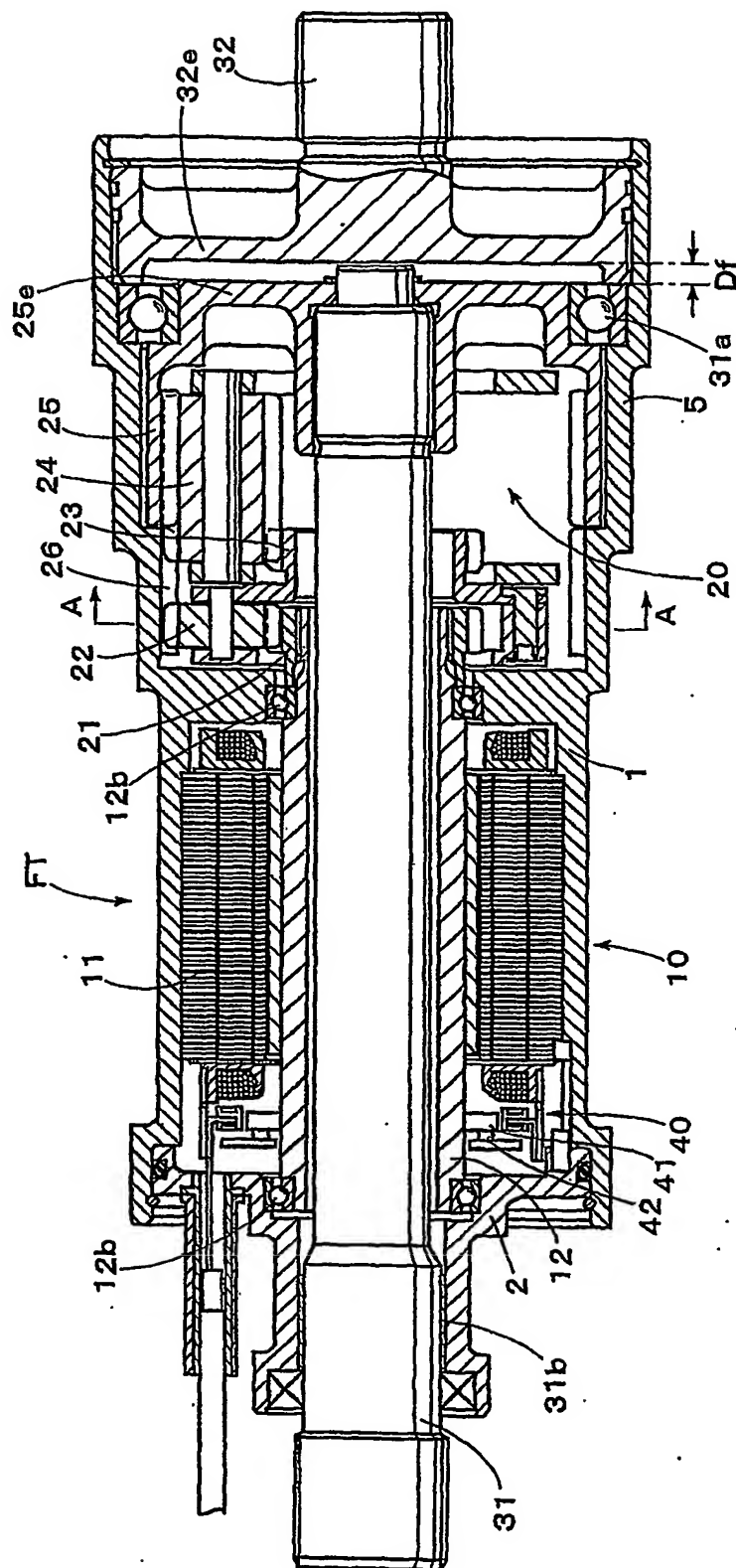


FIG. 5

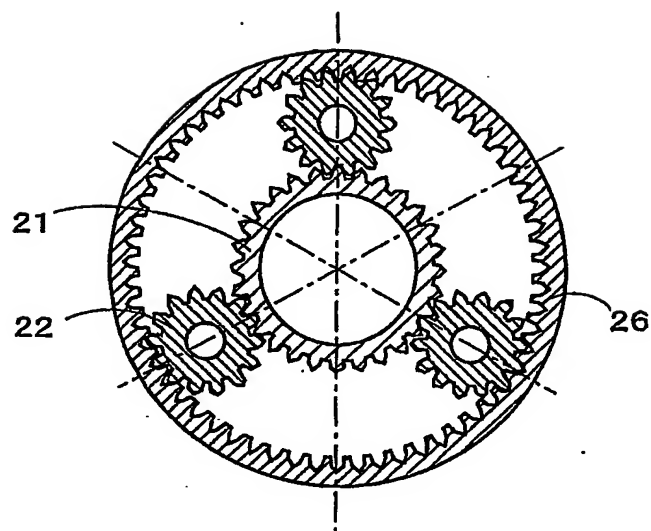


FIG. 6

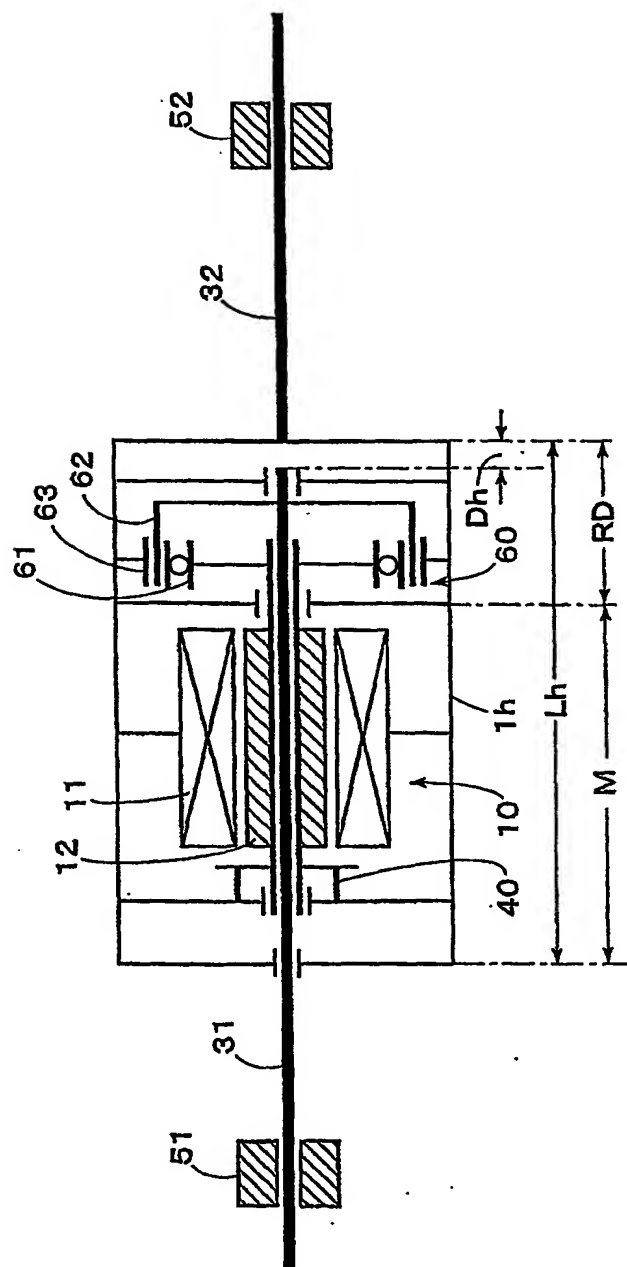


FIG. 7

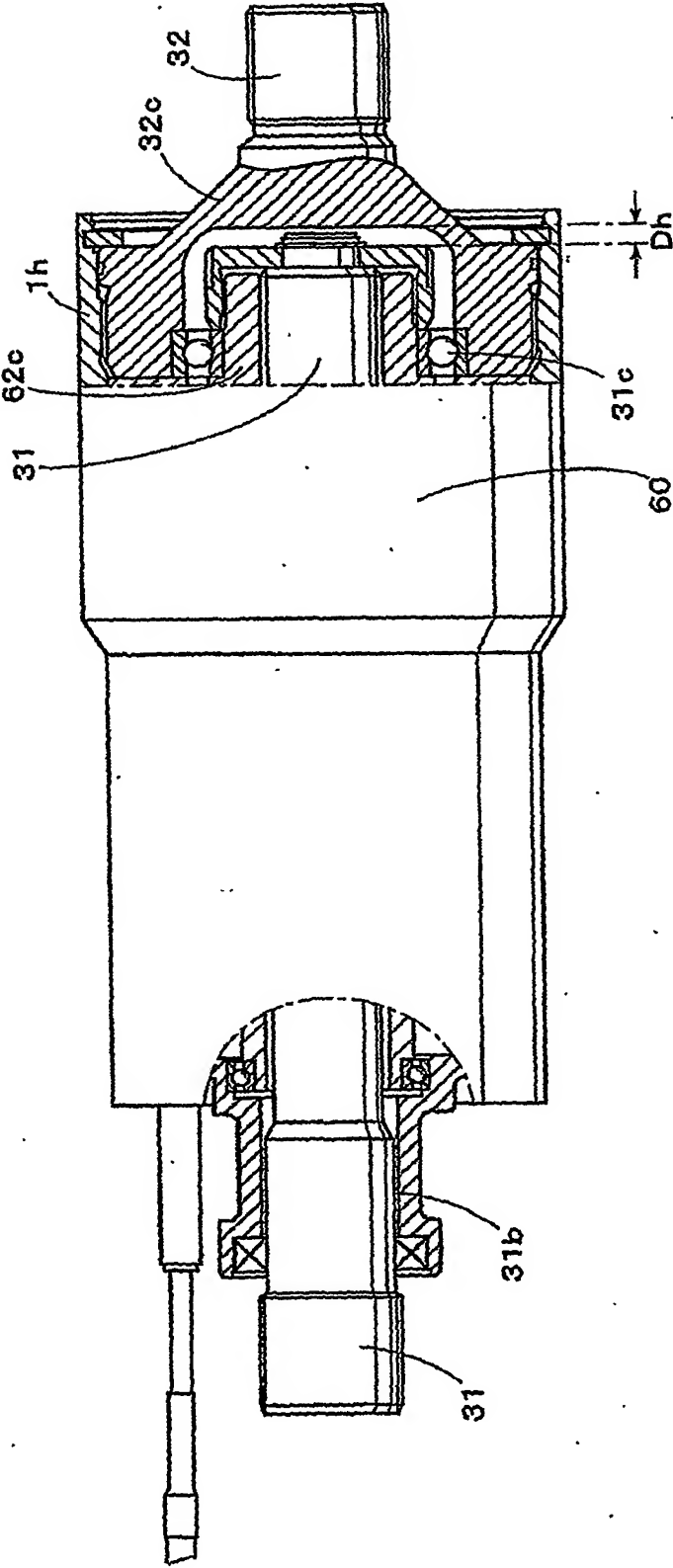


FIG. 8

